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# Dielectric and piezoelectric properties of  $Cu<sup>2+</sup>$ -doped alkali Niobates

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### **Abstract**

The effect of  $Cu^{2+}$  addition  $(0.5-2 \text{ mol%)}$  on microstructure and electromechanical properties of lead-free piezoelectric system of  $(K_{0.44}Na_{0.52}Li_{0.04})(Ta_{0.1}Sb_{0.06}Nb_{0.84})O_3$  (KNN-LT-LS) was investigated through two processing methods; namely perovskite and mixed-oxide. The addition of  $Cu^{2+}$  showed an increase in grain size and relative density of the undoped ceramics in both processing techniques. Introduction of  $Cu<sup>2+</sup>$  stabilized the orthorhombic phase at room temperature by shifting the tetragonal–orthorhomic phase transition to higher temperatures while did not show any major changes in  $T_c$ . The polarization-field response of Cu<sup>2+</sup>-doped ceramics showed a decline in both remnant polarization and coercive field, thus reducing the area of the hysteresis loop. This shrinkage in hysteresis loop was manifested through a large improvement in mechanical quality factor, nearly 4 times that of undoped ceramic. Within the studied range of  $Cu^{2+}$  addition, the ceramic with 0.5 mol% of  $Cu^{2+}$ prepared by mixed-oxide route represented a relatively desirable balance between the degradation of the electromechanical properties, improvement in temperature stability, and mechanical quality factor.

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# **1. Introduction**

Lead-free piezoelectric materials were utilized in applications prior to the introduction of lead zirconate titanate [PZT or Pb( $Zr_{1-x}$  $Zr_{1-x}$  $Zr_{1-x}$ ,Ti<sub>x</sub>)O<sub>3</sub>] in the 1950s in Japan.<sup>1</sup> Lead based materials are more widely used as piezoelectric materials in transducer devices due to their superior electromechanical properties.<sup>[2](#page-6-0)</sup> Despite this, the high lead content in their compositions has raised environmental and safety concerns regarding proper han-dling, disposal and recycling.<sup>[3,4](#page-6-0)</sup> Legislation on electrical and electronic equipment waste and restriction of hazardous substances (RoHS) has been recently enforced as the directive in the European Union $5-8$  which may highly impact piezoelectric manufactures in future. In fact, this global action has sparked enough momentum for scientists to search for lead-free alternative materials with comparable dielectric and electromechanical properties to their lead-based counterparts.

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Among different lead-free compositions, potassium sodium niobate  $(K_{0.5}Na_{0.5}NbO_3; KNN)$  solid solutions have shown promising electromechanical properties comparable with lead-based piezoceramics.<sup>[9](#page-6-0)</sup> The potassium sodium niobate (KNN) composition is composed of equi-molar solid solution of KNbO<sub>3</sub>  $(KN)$  and NaNbO<sub>3</sub> (NN).<sup>[1,10,11](#page-6-0)</sup> Both KN and NN demonstrate orthorhombic symmetry at room temperature. Although the former shows ferroelectric behavior, the latter demon-strates an anti-ferroelectric response.<sup>[12](#page-7-0)</sup> Pioneering works on the binary and ternary compositions of  $KNN-LiTaO<sub>3</sub>$  and  $KNN-LiTaO<sub>3</sub>-LiSbO<sub>3</sub>$  reported by Saito et al., have explicitly shown that the piezoelectric properties comparable to MPB of PZT, as well as barium and lanthanum doped PZT, can indeed be achieved.<sup>[9,13–15](#page-6-0)</sup> The piezoelectric charge coefficient of the binary system falls in the range of 150–230 pC/N and the ternary system shows a  $d_{33} = 300$  pC/N, with their Curie temperatures of being in 170–500 and 253 ◦C, respectively. The substitution of the  $Sb^{5+}$  and Ta<sup>5+</sup> in octahedral sites of NbO<sub>6</sub> in the ternary system of KNN-LT-LS gives rise to a "soft" ferroelectric behavior, which improves the piezoelectric and coupling coefficients while increasing dielectric loss and reducing the mechanical quality factor.

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The improved electromechanical properties of KNN-LT-LS ceramics make them suitable candidate as soft lead-free ferroelectric materials for actuators, sensors,  $low^{16}$  $low^{16}$  $low^{16}$  and high frequency<sup>[17](#page-7-0)</sup> ultrasonic transducer devices. However, the usage of this ternary system is undesirable for high power transducer applications, due to the instability of its coupling coefficients with small temperature variations, its high dielectric loss (tan  $\delta$ : 1.7–4%) and low mechanical quality factor  $(Q_m: 50-85)$ . Introducing additives is an effective way of minimizing the temperature sensitivity, reducing the dielectric loss, and enhancing mechanical quality factor. Previous researchers have shown that the addition of  $Cu^{2+}$  to alkali niobate systems results in an improvement in sinterability, microstructure texturing and mechanical quality factor.[18–21](#page-7-0)

The objective of the present study was to demonstrate the effect of  $Cu^{2+}$  addition on the microstructure, phase transition, crystal structure, and electromechanical properties of  $(K_{0.44}Na_{0.52}Li_{0.04})(Ta_{0.1}Sb_{0.06}Nb_{0.84})O_3$  system in order to be used as a "hard" ferroelectric material for high power ultrasonic transducers.

### **2. Experimental procedure**

The compositions of interest were synthesized by two processing routes of perovskite and mixed-oxide according to the chemical formula of  $(K_{0.44}Na_{0.52}Li_{0.04})(Ta_{0.1}Sb_{0.06}$  $Nb<sub>0.84</sub>$ )O<sub>3</sub> + *x*CuO, where *x* is the mole fraction of the Cu<sup>2+</sup> dopant  $(x=0.0, 0.5, 1.0, 1.5, 2.0)$ . The details of powder processing and synthesis are described in Ref. [22.](#page-7-0) The prepared powders were uni-axially pressed and sintered at 1150 ◦C for 1 h in an oxygen atmosphere (O<sub>2</sub> flow rate of  $360 \text{ cm}^3/\text{min}$ ). The top and bottom surfaces of the pellets were polished down to about 0.5 mm and Au electrode was deposited by DC sputtering. The samples were poled under an electric field of 30 kV/cm for 15 min in a silicon oil bath at  $100\,^{\circ}$ C.

The microstructures of the sintered samples were studied by field emission scanning electron microscopy (FESEM) LEO (ZEISS) 982. Grain size measurements were carried out using the mean intercept length method from different areas of the sample. Qualitative X-ray phase analysis was carried out on Xray diffractometer Philips D500 with Cu  $K_{\alpha}$  radiation using a step-scan of  $0.03°$ /step in  $2\theta$  and 1 s dwell time/step. Piezoelectric charge coefficient,  $d_{33}$ , was directly recorded from a Berlincourt piezometer (Channel Products, Inc.) by averaging ten readings from each surface of the ceramic pellets. Poisson's ratio was measured from the ratio of the first overtone to the fundamental resonance frequency  $(f_s^{(2)}/f_s)$  of the planar mode in accordance to the IEEE standards.<sup>[23](#page-7-0)</sup> Piezoelectric planar, thickness and the 31 mode coupling coefficients,  $(k_n, k_t, \text{and } k_{31})$  were calculated from the resonance and anti-resonance frequencies of the impedance traces, based on the IEEE standard. Longitudinal coupling coefficient, *k*33, was estimated from the thickness and planar coupling coefficients.<sup>[1](#page-6-0)</sup> Planar and thickness frequency constants were obtained from resonance frequencies of planar  $f_s^p$  and thickness  $f_s^t$  modes, respectively. Using an HP 4194A impedance/gain-phase analyzer, the planar mechanical quality

factor was calculated using<sup>23</sup>:

$$
Q_m = \frac{1}{R} \sqrt{\frac{L}{C_a}}
$$
 (1)

where the  $R$ ,  $L$ , and  $C_a$  are the resistance, inductance and capacitance in the equivalent electrical circuit of the piezoelectric resonator, respectively.

## **3. Results and discussion**

## *3.1. Sintering and microstructural analysis*

The addition of  $Cu^{2+}$  changed the average grain size and grain morphology in both perovskite and mixed-oxide routes as depicted in [Fig. 1.](#page-2-0) Average grain size in undoped ceramics was  $2.5$  and  $3 \mu m$  for perovskite and mixed-oxide routes, respectively. Addition of  $2 \text{ mol} \% \text{ Cu}^{2+}$  increased the average grain size to about  $4 \mu m$  in perovskite and  $5 \mu m$  in mixedoxide routes. Densities of ceramics were also slightly increased and reached 97.6% and 97.3% for perovskite and mixed-oxide routes, respectively. In addition, grain morphology changed from sharp-cornered cubical grains with smooth surfaces to cutcornered grains with rough surfaces. It appeared that introducing the  $Cu^{2+}$  altered the growth behavior of the grains by decreasing the surface energy. Based on the Jackson solid–liquid interface model, high entropy of fusion  $(\Delta S_f > 2R; R: 1.9872 \text{ cal/mol K})$ thermodynamically favors the layer by layer growth and, there-fore, creates atomically smooth growth surface.<sup>[24](#page-7-0)</sup> However, at lower entropy of fusion  $(\Delta S_f < 2R)$ , there is no preferential growth and hence random growth with rough surfaces occurs. It was hypothesized that the addition of  $Cu^{2+}$  decreased the entropy of fusion in KNN-LT-LS system by lowering its surface free energy, thus giving rise to the observed rough surfaces.

## *3.2. Phase analysis*

[Fig. 2](#page-3-0) shows X-ray diffraction patterns of the sintered KNN-LT-LS ceramics with different molar percentages of  $Cu^{2+}$ prepared by mixed-oxide route (X-ray patterns of both routes were quite similar, thus only the mixed-oxide route was selected and discussed here). As shown, the solid solution of  $Cu^{2+}$  in KNN-LT-LS structure was observed with no detectable second phase within the dopant range of  $0-2$  mol%. Li et al.<sup>[20](#page-7-0)</sup> reported the presence of second phase  $K_4$ CuNb<sub>8</sub>O<sub>23</sub> in the Cu<sup>2+</sup> added  $(K_{0.44}Na_{0.52}Li_{0.04})(Ta_{0.1}Sb_{0.04}Nb_{0.86})O_3$  ceramic when the  $Cu^{2+}$  addition exceeded from 0.1 mol%. The disparity in results could be attributed to the slight compositional difference (higher  $Sb^{5+}/Nb^{5+}$  ratio in current study than Li's), different powder precursors, and processing procedure.

The X-ray diffraction pattern of the base composition  $(0\% \text{ Cu}^{2+})$  showed the coexistence of two structures namely orthorhombic and tetragonal phases at room temperature. Introducing  $Cu^{2+}$  in the range of  $0 < x < 1.0$  mol% stabilized the orthorhombic structure. Further increase in concentration of  $Cu^{2+}$  beyond 1.0 mol% reduced the splitting of (220) and

<span id="page-2-0"></span>

Fig. 1. SEM microstructure of the 0, 0.5, 1, 1.5, and 2 mol% Cu-doped KNN-LT-LS ceramics prepared through (a–e) "perovskite" and (f–j) "mixed-oxide" routes.

(0 0 2) orthorhombic reflections. This implied that the dopant was still incorporated into the perovskite structure in the form of solid solution even at doping level of 2 mol%. At 1.5 and 2 mol%  $Cu^{2+}$  concentrations, merging of (2 2 0) and (0 0 2) was observed, seemingly pointing to a phase transition to tetragonal. While it did not match with tetragonal structure, the X-ray pattern suggested that the transition leaned favorably toward distorted orthorhombic. This observation was also confirmed by permittivity–temperature measurements which will be discussed in Section [3.3.](#page-3-0)

<span id="page-3-0"></span>

Fig. 2. X-ray diffraction patterns of the 0, 0.5, 1, 1.5, and 2 mol%  $Cu^{2+}$ -doped KNN-LT-LS ceramics prepared by "mixed-oxide route".

# *3.3. Temperature dependence of relative permittivity and dielectric loss*

Temperature dependence of relative permittivity and dielectric loss were measured upon cooling at the frequency of 1 kHz in the temperature range of  $0-380$  °C. As illustrated in Fig. 3a and b, both perovskite and mixed-oxide routes showed similar temperature–permittivity behaviors with three distinctive



Fig. 3. Temperature dependence of relative permittivity and dielectric loss, upon  $Cu<sup>2+</sup>$  addition on KNN-LT-LS ceramics prepared by (a) "perovskite" and (b) "mixed-oxide" route. Measured frequency: 1 kHz.



Fig. 4. Temperature dependence of permittivity for  $Cu^{2+}$ -doped KNN-LT-LS ceramics prepared by mixed-oxide route and measured at 1 kHz.

regions separated by two phase transitions. For undoped ceramics, the orthorhombic–tetragonal  $(T_{o-t})$  and tetragonal–cubic (Curie temperature;  $T_c$ ) phase transitions occurred at ∼34 and 264  $\rm{^{\circ}C}$ , respectively. Relative permittivity peaks at  $T_c$  were sharp and had the highest value for undoped ceramic. Addition of the  $Cu^{2+}$  gave rise to a sharp decrease in  $K_{max}$  without affecting the Curie temperature. This is in good agreement with the results reported for  $Cu^{2+}$ -doped alkali niobate systems on lowering per-mittivity especially at the Curie point. Saito and Takao<sup>[18](#page-7-0)</sup> and Lin et al. $^{21}$  $^{21}$  $^{21}$  reported the insensitivity of Curie temperature to the introduction of 0.01 and 1 mol%  $Cu^{2+}$  to KNN. However, Li et al. observed a slight change in  $T_c$  ( $\sim$ 4 °C upon 0.3 wt% Cu<sup>2+</sup>).<sup>[20](#page-7-0)</sup>

Despite the insensitivity of the  $T_c$  to the addition of  $Cu<sup>2+</sup>$ , the room temperature phase transition temperature (orthorhombic–tetragonal;  $T_{o-t}$ ) shifted toward higher temperature upon addition of  $Cu^{2+}$  in both processing techniques (Fig. 4). The increase in room temperature transition point  $(T_{o-t})$ was up to 22 and 24 ℃ for both pervoskite and mixed-oxide routes, respectively. Introducing higher  $Cu^{2+}$  (1.5 and 2 mol%) contents to the structure of the KNN-LT-LS resulted in diffuse phase transition shown by wider permittivity peak. Temperature dependence of dielectric loss showed the similar trend of changes in both processing methods. At temperatures  $\langle 175 \degree C$ , the  $Cu<sup>2+</sup>$ -doped ceramics had lower dielectric loss compared to the undoped ceramic. While at the temperatures  $>175$  °C and particularly above  $T_c$ , the addition of  $\overline{\text{Cu}}^{2+}$  resulted in a sharp increase in dielectric loss values and shifting the loss patterns toward room temperature. This was mainly due to a decrease in bulk resistivity of KNN-LT-LS ceramics at higher temperatures, where the ceramic becomes electrically conductive.

# *3.4. Electromechanical properties*

Room temperature dielectric properties of  $Cu^{2+}$ -doped KNN-LT-LS ceramics are shown in [Fig. 5a](#page-4-0) and e. Addition of  $Cu^{2+}$  up to 0.5 mol% to the base compositions, drastically decreased both relative permittivity and dielectric loss (33% and 67%, respectively; in perovskite route). Further addition

<span id="page-4-0"></span>

Fig. 5. Effect of  $Cu^{2+}$  addition on dielectric and piezoelectric properties of  $Cu^{2+}$ -doped KNN-LT-LS ceramics prepared through (a–d) "perovskite" and (e–h) "mixed-oxide" routes.

of  $Cu^{2+}$  (>0.5 mol%) resulted in a gradual decline of relative permittivity.

The sharp decline of dielectric loss was accompanied by an abrupt rise in mechanical quality factor. The mechanical quality factor measured at minimum impedance  $|Z_m|$  of the fundamental resonance is generally defined as the ratio of in-phase strain to out-of-phase strain with stress, and analogous to electrical quality factor, is inversely related to dielectric loss or dissipation factor. Since the extent of the mechanical *Q* is determined by the presence of the movable domain walls, the energy loss from the domain wall motions suppresses the mechanical vibration of the resonator. This mechanical damping which is converted into heat lowers the  $Q_m$  value and increases the dissipation factor. It appears that the addition of  $Cu^{2+}$  has reduced the energy loss of the KNN-LT-LS system by restricting the domain wall motions and causing less interference with mechanical vibration of the ceramic resonator. The high *Qm* is desirable especially for high power ultrasonic applications, where the energy loss and generated heat are critical factors affecting the performance of transducer.

The relationship between mechanical *Q* and dielectric loss can be clearly seen from the sharp incline in  $Q_m$  values due to the drastic decrease in dissipation factor. As illustrated in Fig. 5b and f, notable improvement (three times more than those of undoped ceramics) in mechanical quality factor was achieved at 0.5 mol%  $Cu^{2+}$ . At higher concentrations of additive (>0.5 mol%), the rate of increase was not that significant and approached a linear type of variation (from  $0.5$  to  $2 \text{ mol} \%$ ). Meanwhile, improvement in mechanical quality factor was the highest at 2 mol% additive (about five times that of undoped ceramic). Fig. 5c and g depicts piezoelectric charge and coupling coefficients of  $Cu^{2+}$ doped KNN-LT-LS ceramics. The addition of  $Cu^{2+}$  lowered both piezoelectric charge and longitudinal coupling coefficients. In addition, introduction of the additive had a pronounced effect on reducing the *d*33. The decrease in piezoelectric charge coefficient could be due to the "hardening" effect, which lowers the piezoelectric charge and coupling coefficients, as well as the dielectric loss. It is believed that the decline in piezoelectric properties upon  $Cu^{2+}$  addition was due to the stabilization of orthorhombic phase at room temperature. This would consequently contribute to a smaller number of possible polarization directions. The effect of  $Cu^{2+}$  addition on thickness and planar coupling coefficients are shown in Fig. 5d and h.

## *3.5. Polarization-field response in doped KNN-LT-LS*

[Fig. 6a](#page-5-0) and b illustrates the room temperature field dependence of polarization for  $Cu^{2+}$ -doped KNN-LT-LS ceramics measured at 50 Hz. The incorporation of  $Cu^{2+}$  lowered the hysteresis loop with regards to undoped ceramic. The hysteresis loop in polarization-field response of a piezoelectric resonator represents the energy required to switch the meta-stable dipole moments during the short application of E-field. The larger the area of hysteresis loop, the higher the energy required to reverse dipoles. In fact, the area of hysteresis shows the amount of dissipated energy in the form of heat. Addition of  $Cu^{2+}$  lowered the

<span id="page-5-0"></span>

Fig. 6. Polarization-field response of the  $Cu^{2+}$ -doped KNN-LT-LS ceramics prepared from (a) perovskite and (b) mixed-oxide routes.

hysteresis area, and therefore the amount of dissipated energy. The effect of  $Cu^{2+}$  addition on dissipation factor (dielectric loss) was already shown in [Fig. 5a](#page-4-0) and e. It appeared that the results of polarization-field were in good agreement with the dielectric loss measurements. This implied that the 0.5 mol%  $Cu^{2+}$  was the most effective dopant concentration, as it facilitated the domain wall switching and led to the lower dissipation factor.

Fig. 7 summarizes the effect of  $Cu^{2+}$ on the polarization and coercive field of KNN-LT-LS ceramics. As shown, the coercive fields for both processing techniques comparatively decreased at similar rates. Typical hard ferroelectrics are known for their relatively low dielectric loss, high mechanical *Q* and high coercive field which are obtained by B-site acceptor substitution. Substitution of the lower valence cation in higher valence B-site induces the oxygen vacancies in the microstructure. These oxygen vacancies reduce the volume of the cell and are believed to play a major role in the 'hardening' effect.<sup>[1](#page-6-0)</sup> In the current  $Cu^{2+}$ doped system, the ionic radius of  $Cu^{2+}$  with coordination number of 6 ( $r_{\text{Cu2+}}$ : 0.87 Å) falls in the size range of A-site ( $r_{K^+}$ :  $1.52 \text{ Å}$ ,  $r_{\text{Na}^+}$ :  $1.16 \text{ Å}$ ,  $r_{\text{Li}^+}$ :  $0.90 \text{ Å}$ ) and B-site  $(r_{\text{Nb}^{5+}})$ : 0.64 Å,  $r_{Ta^{5+}}$  : 0.64 Å,  $r_{Sb^{5+}}$  : 0.60 Å) positions.<sup>[20](#page-7-0)</sup> Based on ionic size, pauling's rules and the fact that perovskite structures have a relatively compact structure with less possibility



Fig. 7. Effect of  $Cu^{2+}$  addition on remnant polarization  $P_r$  and coercive field  $E_c$  of KNN-LT-LS ceramics prepared through "mixed-oxide" and "perovskite" routes. MO: mixed-oxide and P: perovskite.

of interstitial site occupancy, the  $Cu^{2+}$  ion could substitute in either A- or B-site locations. By considering these two possi-bilities one can write the Kroeger–Vink's notation<sup>[25](#page-7-0)</sup> for each process of  $Cu^{2+}$  substitution in A and B sites as:

$$
CuO \to Cu_A^{\circ} + O_o + V_A' \tag{2}
$$

$$
2CuO \rightarrow 2Cu''_B + 2O_o + 3V_o^{\circ\circ}
$$
 (3)

In A-site substitution (Eq. (2)),  $Cu^{2+}$  replaces the K<sup>+</sup>, Na<sup>+</sup>, or  $Li<sup>+</sup>$  cations (designated by A) which induces the A-site vacancy in the structure. This reaction process might be favorable due to the high volatility of the  $Li^+$ ,  $K^+$ , and  $Na^+$  especially above  $1000\degree C^{26-28}$  The B-site substitution (Eq. (3)) which  $Cu^{2+}$  replaces the Nb<sup>5+</sup>, Ta<sup>5+</sup>, or Sb<sup>5+</sup> cations in octahedral sites, gives rise to substantial numbers of vacant sites in anion array, 3 oxygen vacancies for two  $Cu^{2+}$  cation substitutions. As it was discussed earlier in this section, this large number of oxygen vacancies was assumed to be responsible for "hardening" effect of the Cu<sup>2+</sup>-doped KNN-LT-LS ceramic. However, it was expected that this would consequently increase the coercive



Fig. 8. Temperature dependence of polarization for  $Cu^{2+}$ -doped KNN-LT-LS ceramics obtained through mixed-oxide process.

<span id="page-6-0"></span>Table 1 Dielectric and electromechanical properties of  $Cu^{2+}$  (0.5 mol%) doped KNN-LT-LS prepared by perovskite and mixed-oxide routes.

Material	$\epsilon_2^I$ / $\epsilon_0$	$\tan \delta$ (%)	$d_{33}$ (pC/N)	$k_p$	$K_t$	$k_{33}$	$k_{31}$	$Q_m$	$N_p$ (Hz.m)	$N_t$ (Hz.m)	$P_r$ ( $\mu$ C/cm <sup>2</sup> )	$E_c$ (kV/cm)
Perovskite $(0.5\% \text{ Cu}^{2+})$	1170		240	0.45	0.44	0.60	0.26	240	3360	3035		6.7
Mixed-oxide $(0.5\% \text{ Cu}^{2+})$	1230		260	0.48	0.46	0.63	0.27	225	3290	2980		6.9

field of the doped ceramic. In contrast, the decrease of coercive field and the improvement of  $Q_m$  implied that  $Cu^{2+}$  could be substituted in both A- and B-sites.

# *3.6. Temperature dependence of polarization*

In order to study the temperature stability of  $Cu^{2+}$ -doped ceramics, the temperature dependence of remnant polarization was measured within the temperature range of  $20-120$  °C. As shown in [Fig. 8](#page-5-0) the undoped ceramics showed higher remnant polarizations at room temperature. In the case of  $Cu^{2+}$ -doped ceramics, despite the lower initial remnant polarization at room temperature, they demonstrated a relatively stable polarization. As illustrated in [Fig. 8, t](#page-5-0)he polarization retention  $(\%)$  at 120 °C relative to those at room temperature for all  $Cu^{2+}$ -doped ceramics was above 70%, while this value for undoped ceramic was only 15%. It was anticipated that the improved polarization stability upon  $Cu^{2+}$ -doping was directly related to the stabilization of orthorhombic phase at room temperature and the hardening effect of  $Cu^{2+}$  in KNN-LT-LS microstructure. The improved polarization stability could also be due to the substitution of  $Cu^{2+}$ especially in B-site which largely affected the domain wall stabilization through the oxygen vacancy increase and manifested in the form of improved *Qm*.

## **4. Summary and conclusions**

The effect of copper  $(0.5-2 \text{ mol\%)}$  on microstructure, phase transition and electromechanical properties of  $(K_{0.44}Na_{0.52}Li_{0.04})$ (Nb<sub>0.84</sub>Ta<sub>0.1</sub>Sb<sub>0.06</sub>)O<sub>3</sub> system was studied through the perovskite and mixed-oxide routes. Introduction of  $Cu<sup>2+</sup>$  to KNN-LT-LS structure increased the grain size and changed the growth behavior of the grains. Addition of  $Cu^{2+}$  also modified the morphology of grains from sharp-cornered cubical grains with smooth surface to cut-cornered grains with rough surfaces. It was anticipated that the addition of  $Cu^{2+}$  lowered the entropy of fusion for KNN-LT-LS system through a decline in its surface free energy. Relative density of  $Cu^{2+}$ -doped ceramics were slightly increased with dopant concentration and reached to about more than 97% (at  $2 \text{ mol} \% \text{ Cu}^{2+}$ ) for both preparation techniques.

Phase analysis of  $Cu^{2+}$ -doped KNN-LT-LS ceramics showed solid solubility up to 2 mol% with no detectable second phase. Addition of Cu<sup>2+</sup> (0 >  $x \ge 1.0$ ) stabilized the orthorhombic phase at room temperature. While at higher doping concentrations the merging of  $(220)$  and  $(002)$  peaks represented the possibility of distorted orthorhombic phase. The addition of  $Cu^{2+}$  did not change the tetragonal–cubic phase transition (Curie temperature,  $T_c$ ); however, it shifted the orthorhombic–tetragonal phase transition to higher temperatures.

Addition of  $Cu^{2+}$  drastically lowered the room temperature dielectric loss (tan  $\delta$ ) and significantly improved mechanical quality factor  $(Q_m)$ . Piezoelectric charge and coupling coefficients (planar  $k_p$ , thickness  $k_t$  and longitudinal  $k_{33}$ ) were slightly degraded upon doping. This is mainly due to the stabilization of the orthorhombic phase at room temperature and the fact that the undoped ceramics benefited from larger number of polaization directions. Field dependence of polarization showed that polarizability level and coercive field for  $Cu^{2+}$ -doped KNN-LT-LS ceramics decreased. As summarized in Table 1, mixed-oxide route with relatively high piezoelectric charge,  $d_{33}$ : 260 pC/N (∼13% lower than undoped ceramic) and longitudinal coupling coefficients of *k*33: 0.63, provided large improvement in *Qm* (∼4 times), drastic decrease in dielectric loss (>50%), and more than 70% retention of remnant polarization at 120 ◦C. The results of this study suggest that the lead-free  $Cu^{2+}$ -doped KNN-LT-LS ceramic might be a good candidate for high power ultrasonic transducer applications.

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